

Use of diffraction in determine the residual stress of HVOF WC-17Co coatings

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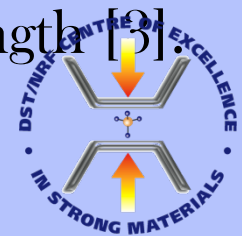
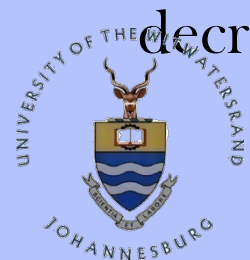
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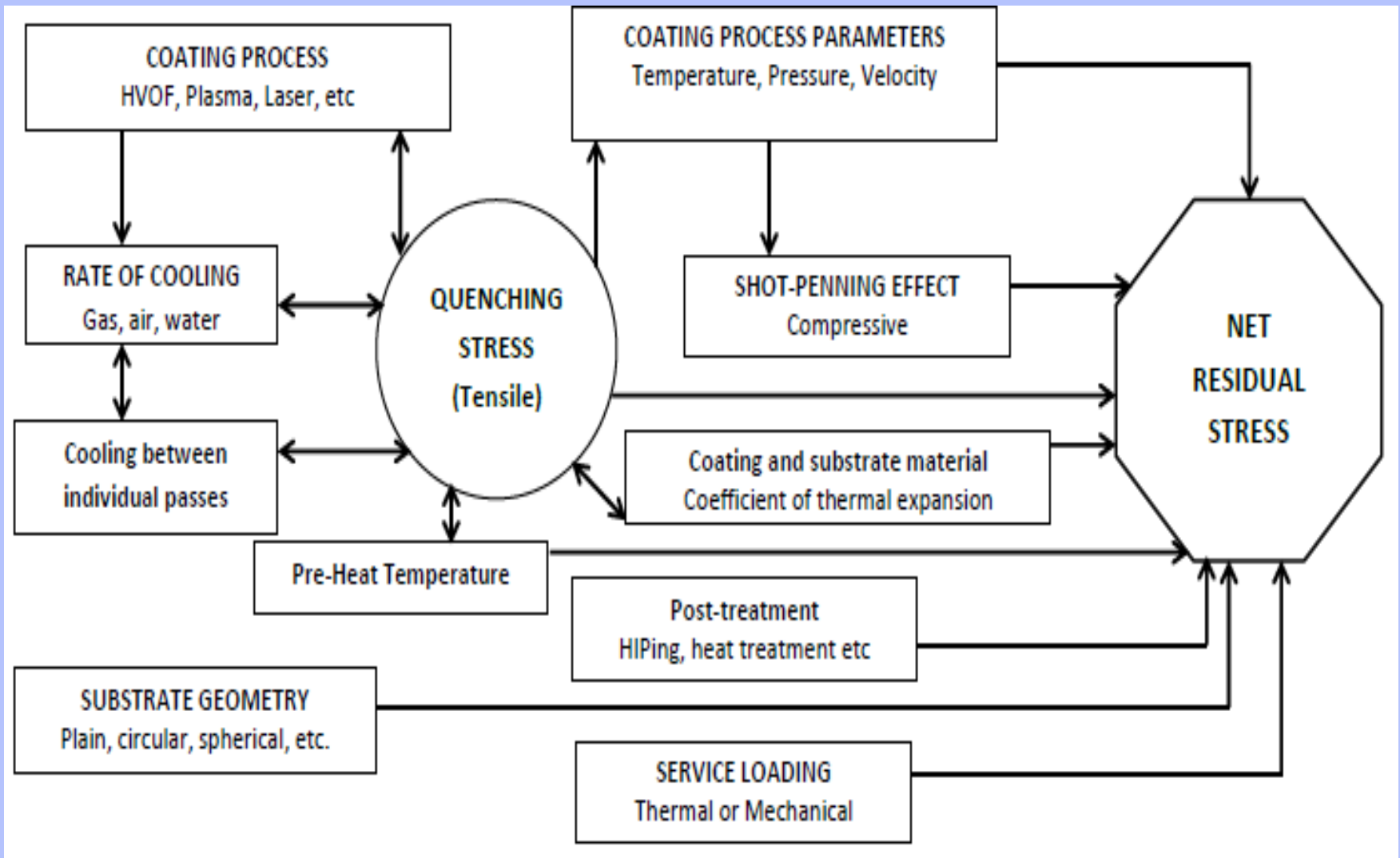


Introduction

- Thermal spray WC-Co coatings protect substrates against different environments and loads e.g. abrasive wear, high temperatures, chemically aggressive fluids and hot gas corrosion.
- WC-Co cermet composites are widely used, owing to their high hardness, reasonable toughness and excellent wear resistance [1].
- Residual stresses are a contributing factor in shortening service life for thermal spray coatings [2].
- Residual stresses in thermal spray coatings are responsible for decreased bending strength, fatigue life and bond strength [3].



Factors influencing the generation of residual stresses in thermal spray coating



Aims and objectives

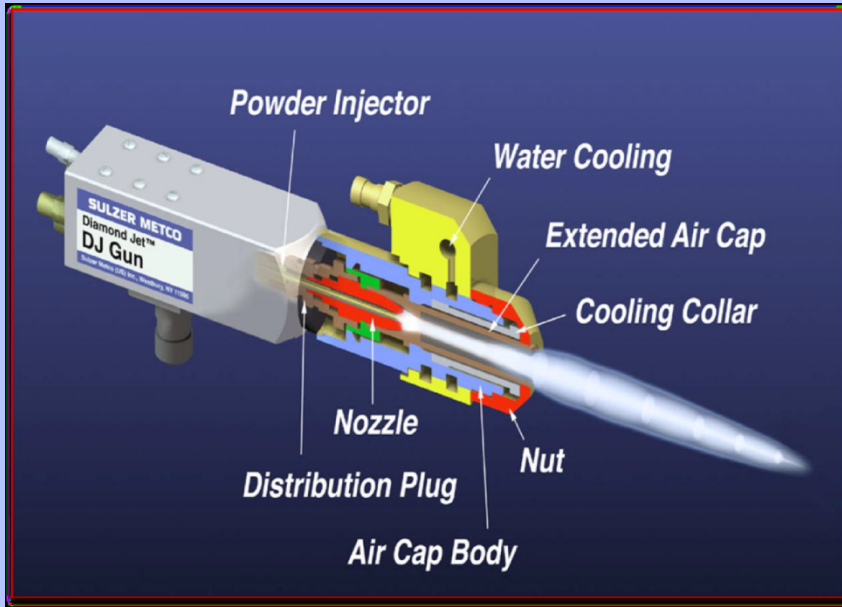
- Identifying & understanding the nature of stresses between the coating and substrate.
- To study the microstructures of HVOF sprayed WC-Co coatings on different metal substrates.
- To explore systematically the residual strains measured by different techniques, i.e. X-ray diffraction, synchrotron XRD and neutron diffraction.
- This project should assist users of coatings in matching substrates and coatings and/or selecting the deposition procedure.



Experimental procedure

- Commercially available WC-17Co powder was used as the feedstock.
- Five different substrates: 304L SS, brass, aluminium, super-invar and mild steel of 25x25x6mm sample size were thermally sprayed by HVOF.
- Samples were studied in: as-sprayed, grit-blasted and annealed grit-blasted conditions.
- XRD, SEM-EDX and Vickers hardness tests were undertaken.
- Stress analyses were carried out by X-ray diffraction, synchrotron XRD and neutron diffraction.

High Velocity Oxy-fuel (HVOF)



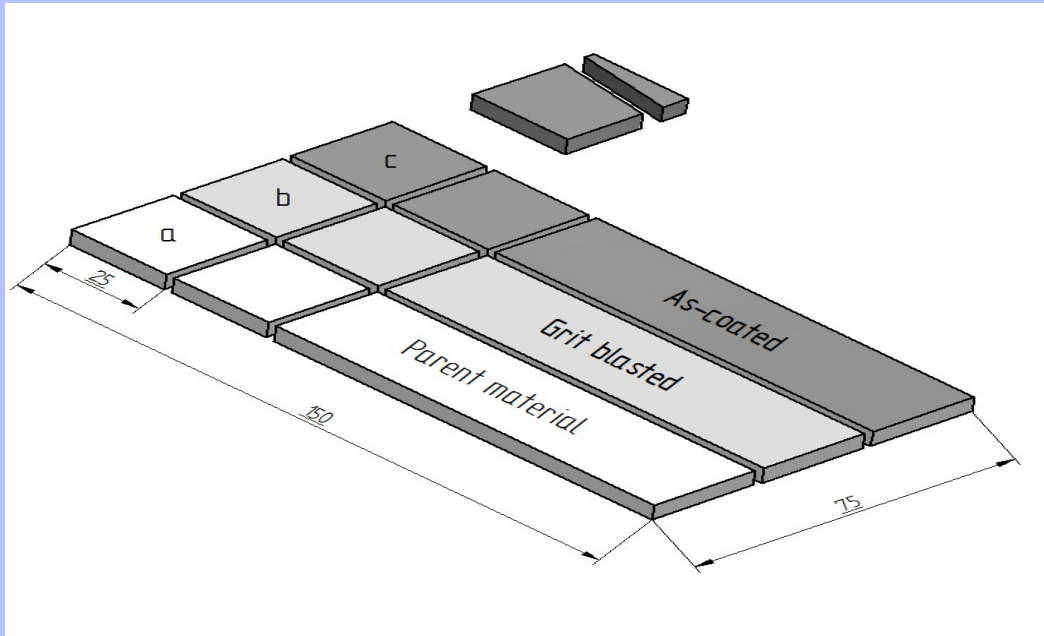
Advantages of HVOF [4]:

- High velocity and low oxygen.
- Lower decarburization.
- Coatings have low porosity and high bond strength.

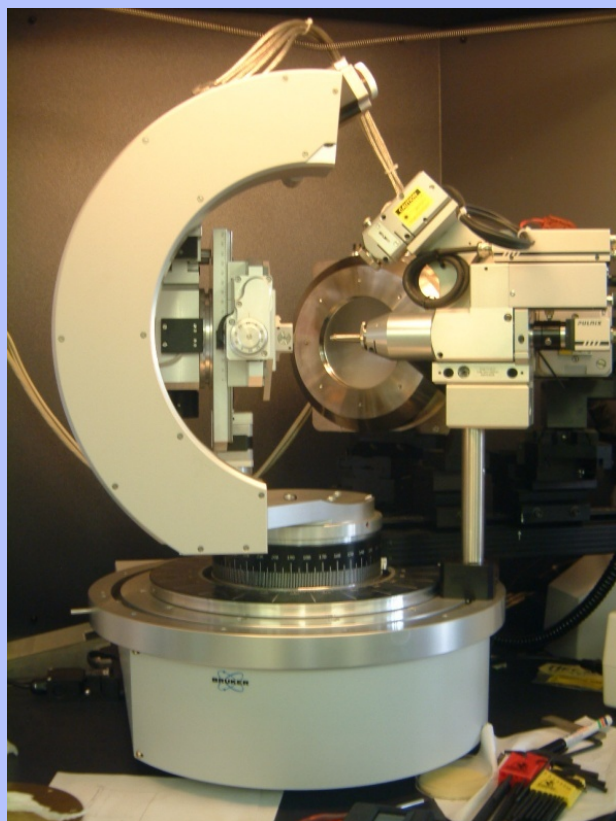
Typically used to deposit wear and corrosion resistant coatings on materials, while protecting from oxidation.



Sample cutting and measuring position



D8 Discover X-ray diffractometer



Sample stage

collimator



Laser video camera

detector

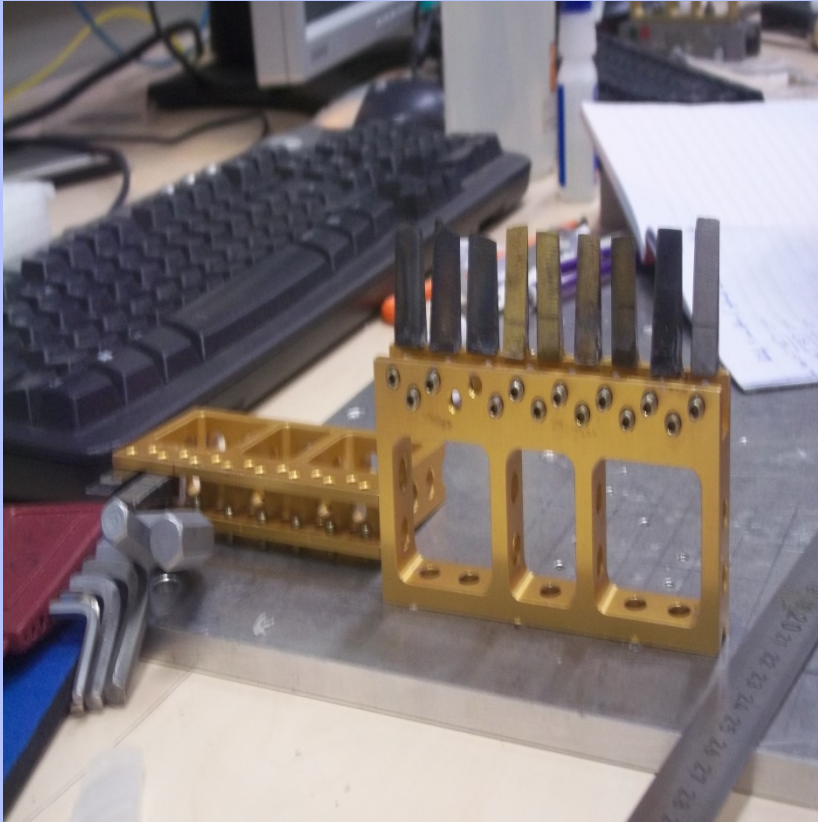
Measurement details

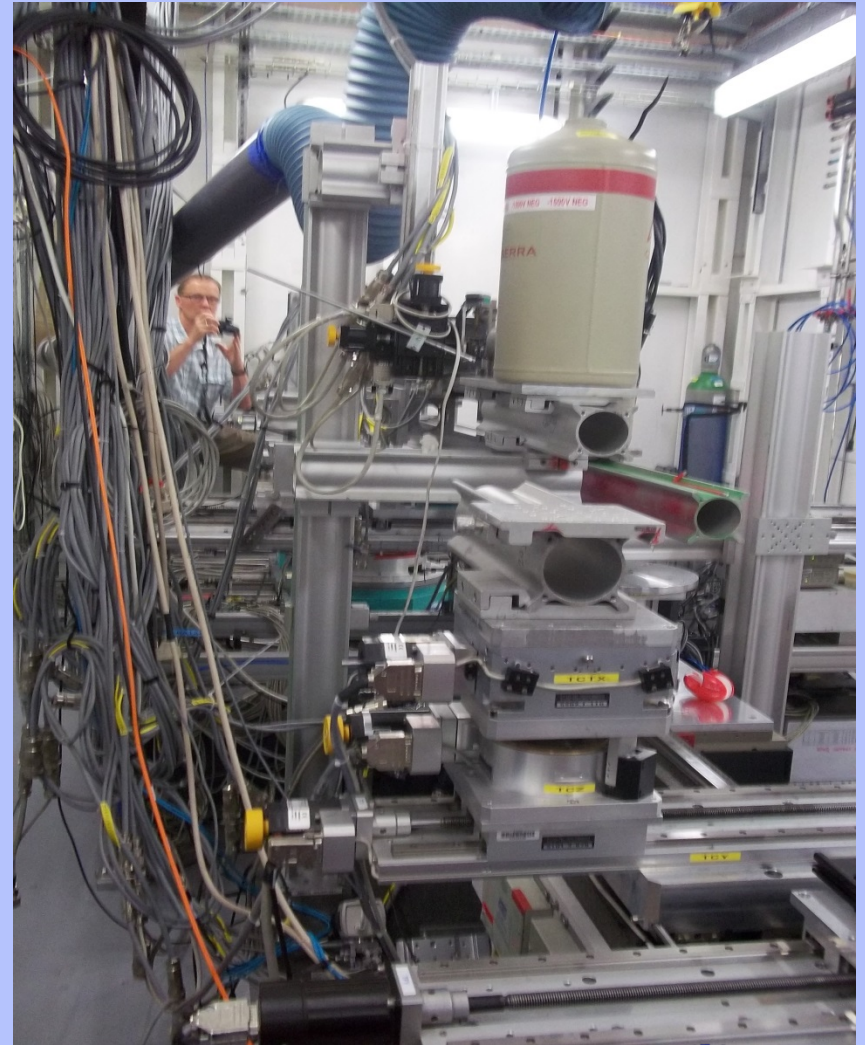
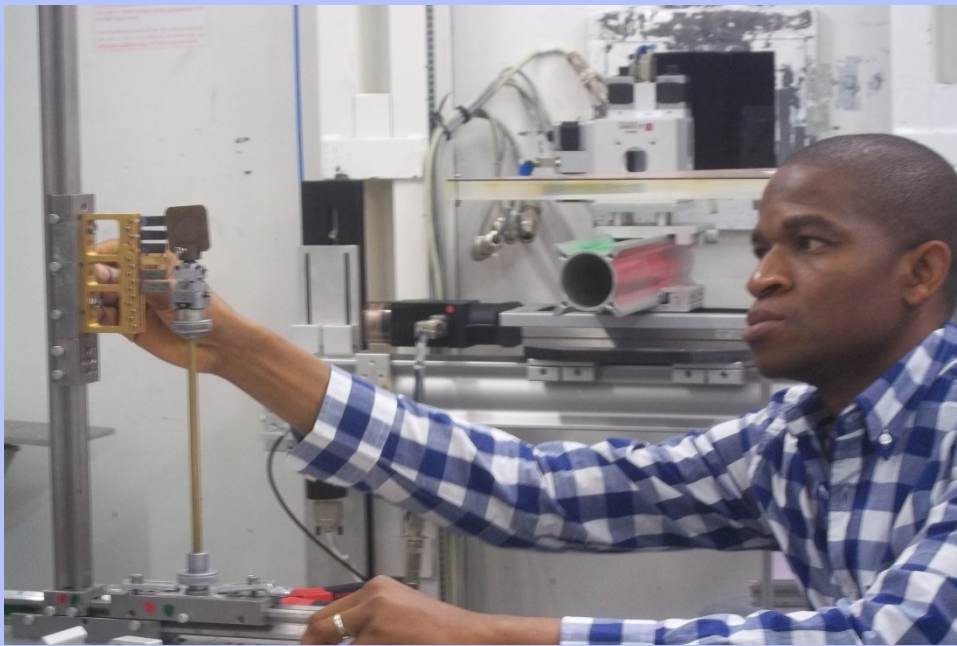
Parameters used:

- Bragg peak: 112_{WC} reflections ($2\varphi = 92.093^\circ$)
- Radiation: Co
- Azimuth orientation ϕ : 0, 180, 90, 270, 45 and 225°
- Tilt angle ψ : $0.0 - 70.0^\circ$
- Steps $\Delta\psi$: 10°
- Software: Leptos V6

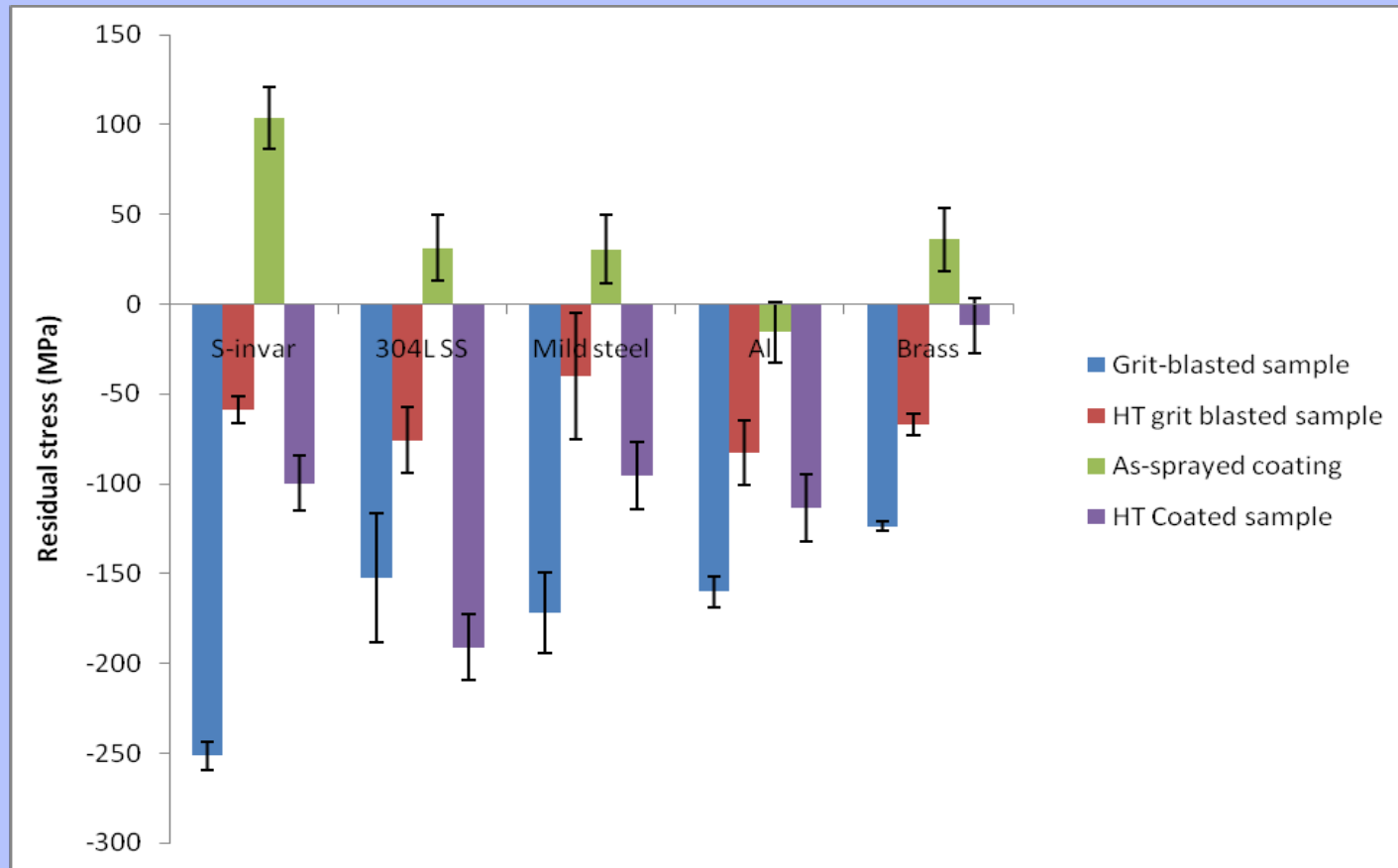


XRD Synchrotron measurement

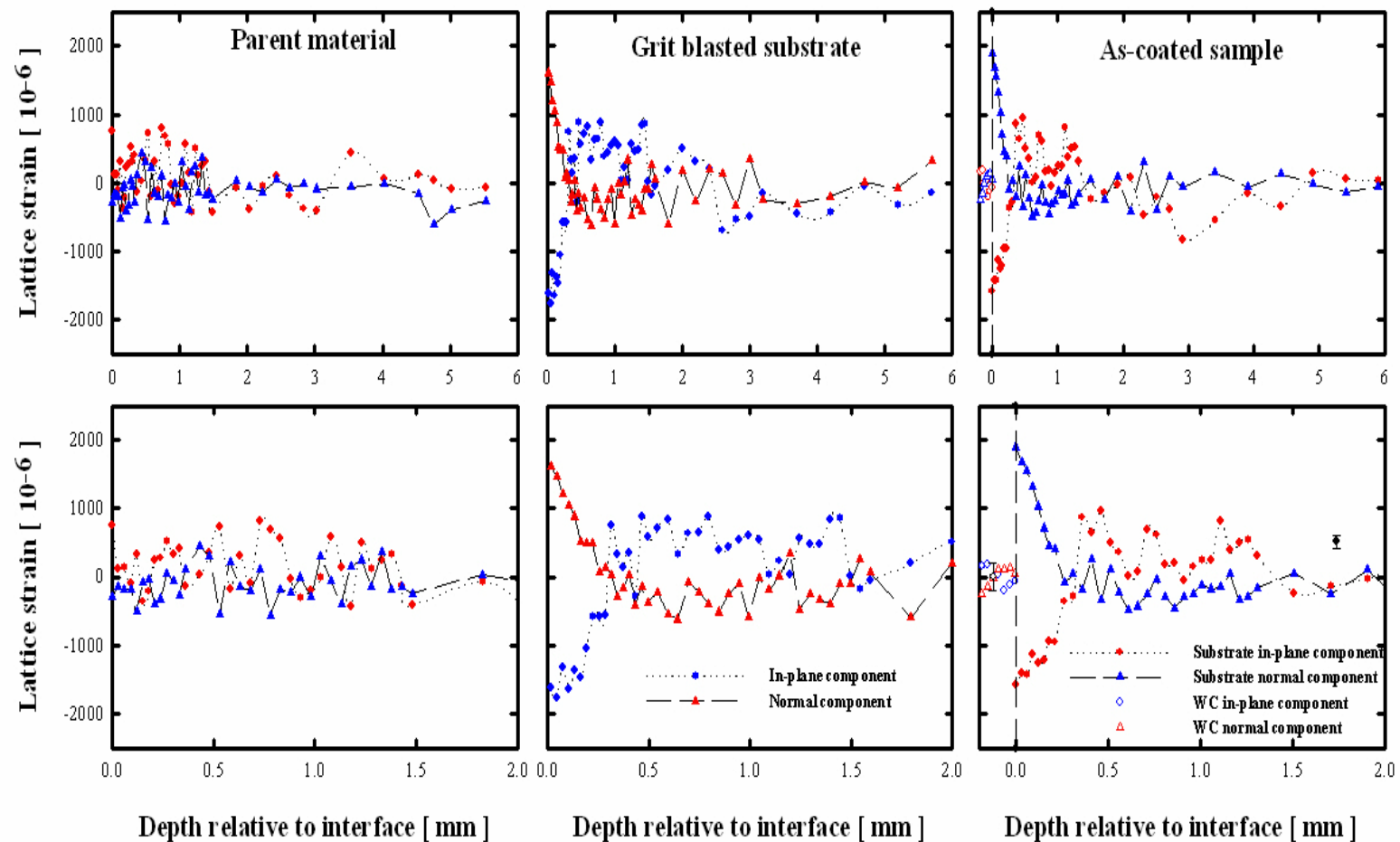




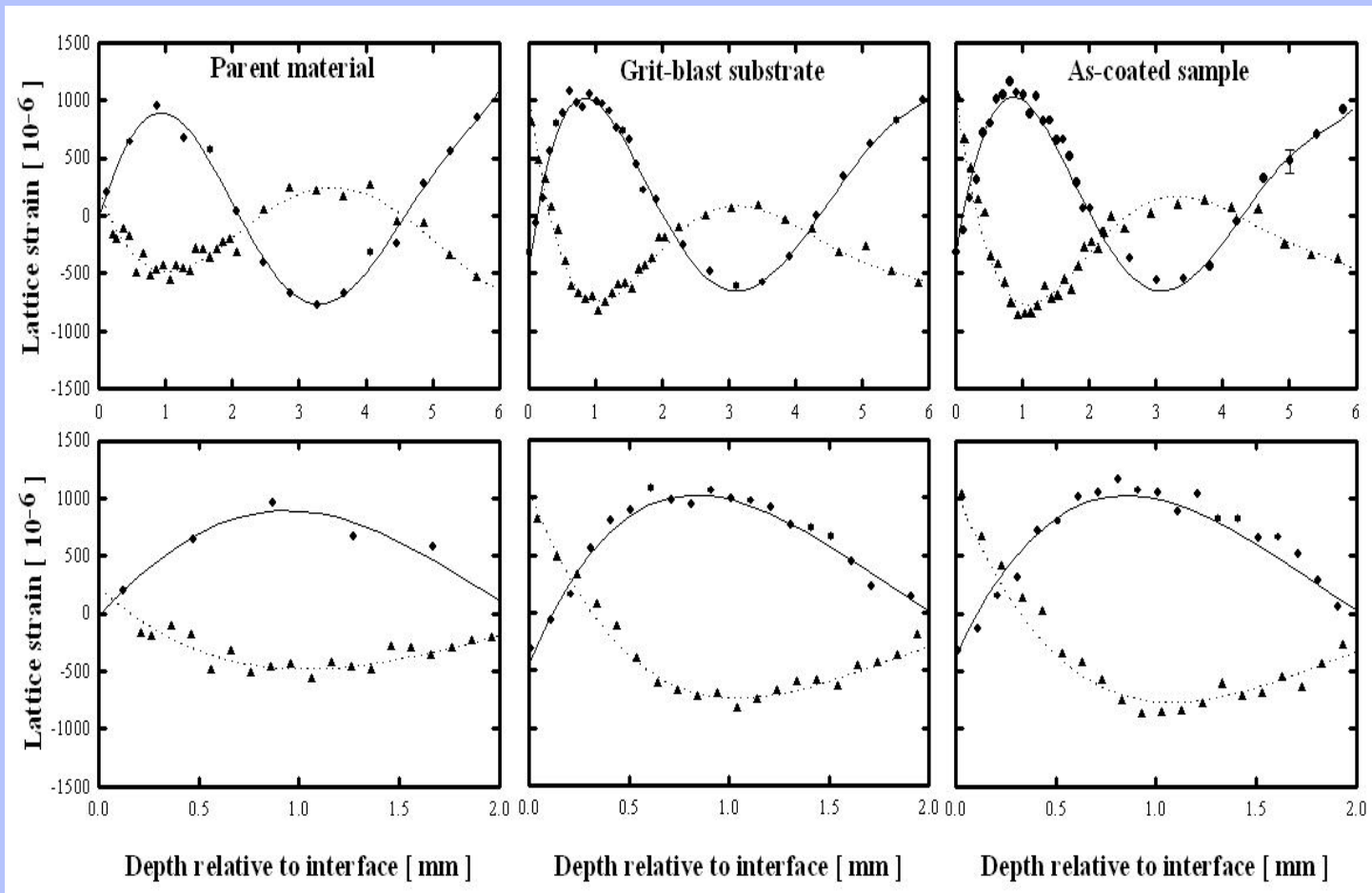
Results and Discussion



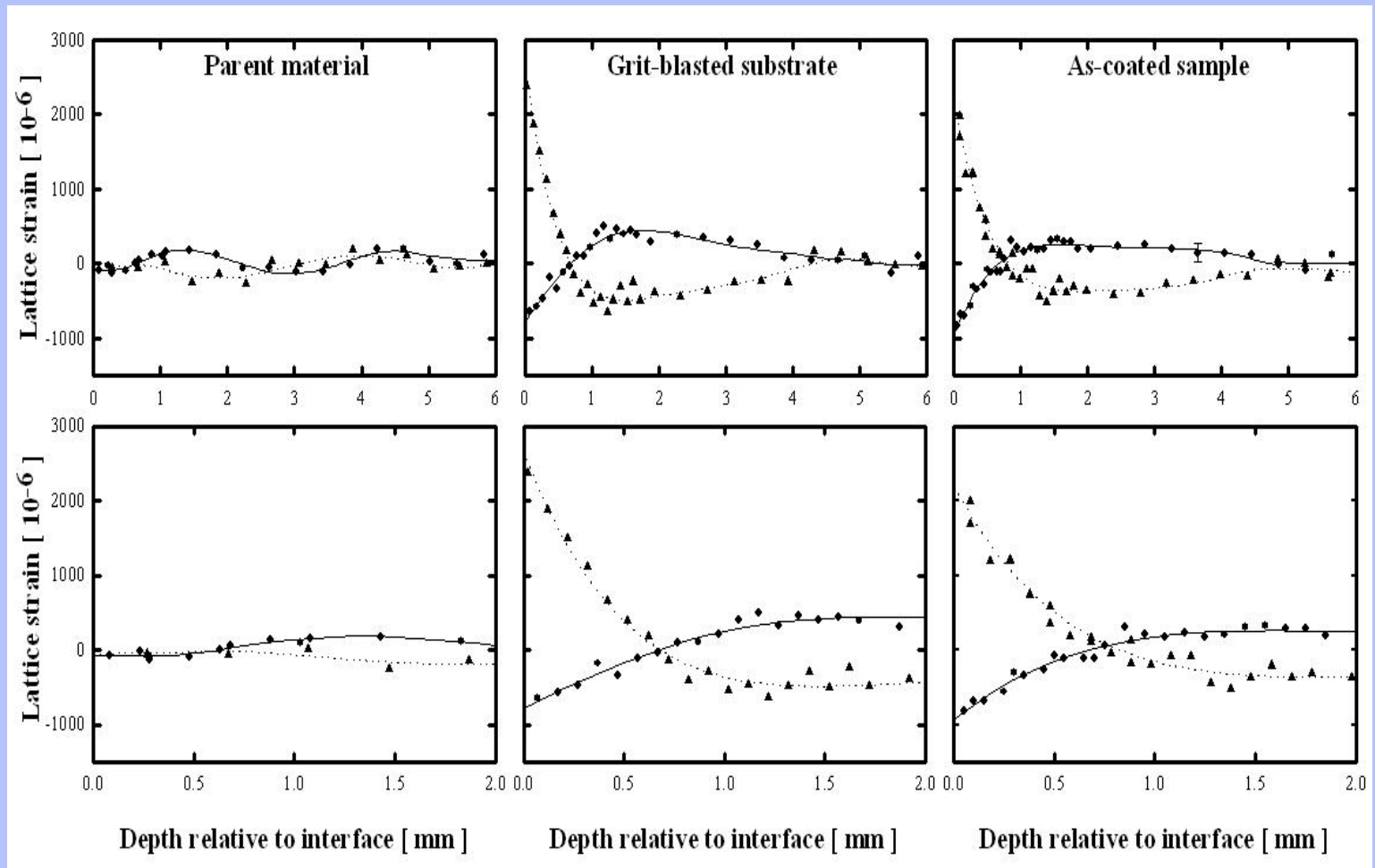
Residual stress of WC-Co coatings measured by X-ray diffraction



Residual strain depth profile for a coated stainless steel

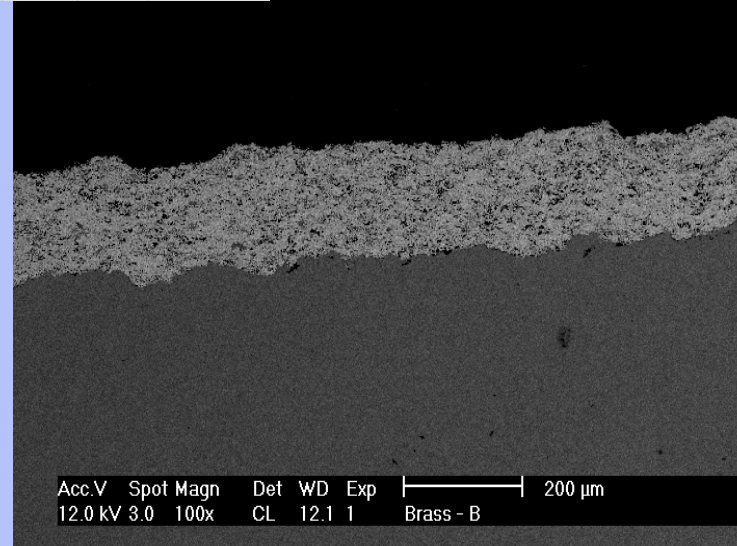
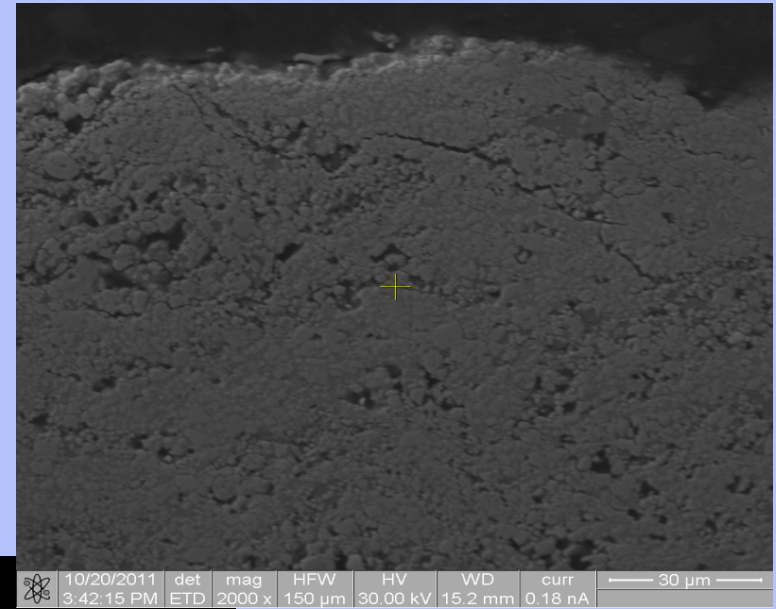
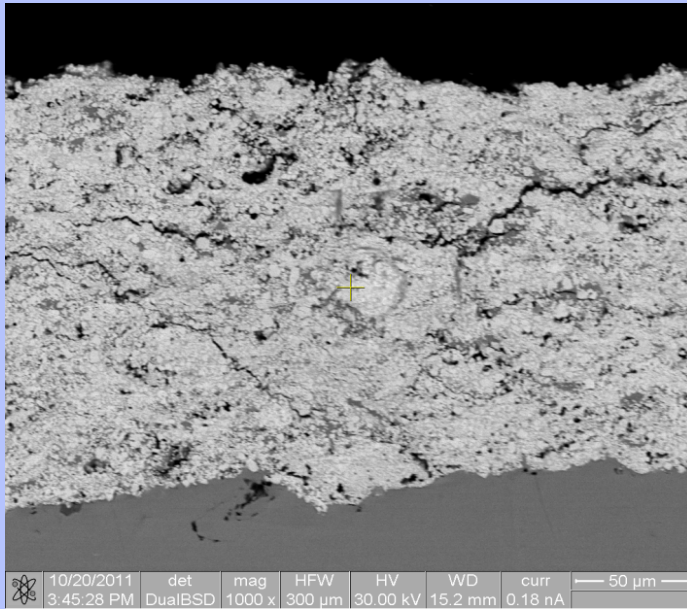


Residual strain depth profile for the coated brass



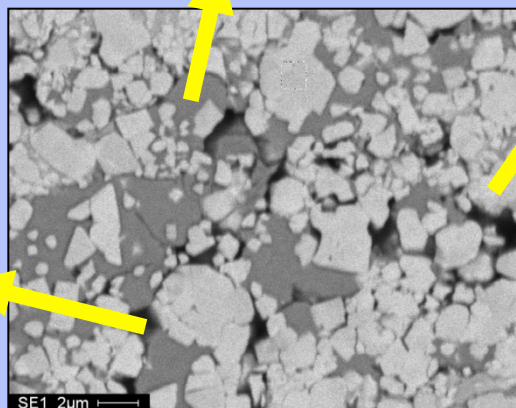
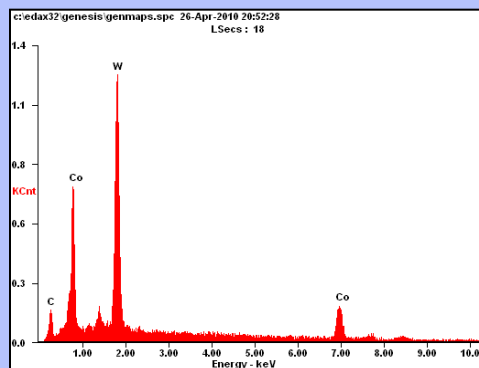
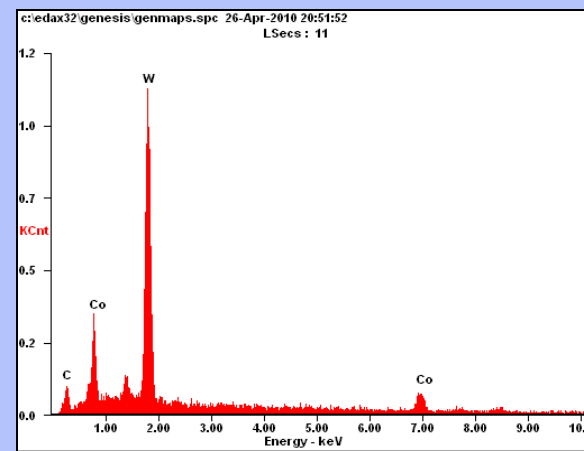
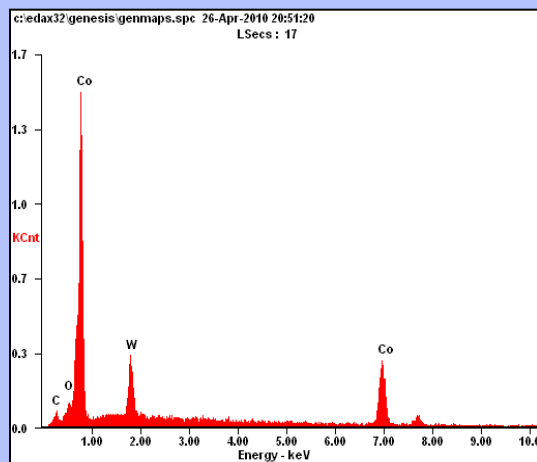
Residual strain depth profile of a coated Super-Invar

Results: Coated brass sample



SEM-BSE images of WC-Co coating on brass substrate.

<i>Element</i>	<i>wt%</i>	<i>at. %</i>
<i>CK</i>	09.1	34.7
<i>OK</i>	03.8	10.9
<i>WM</i>	25.8	06.5
<i>CoK</i>	61.4	47.9

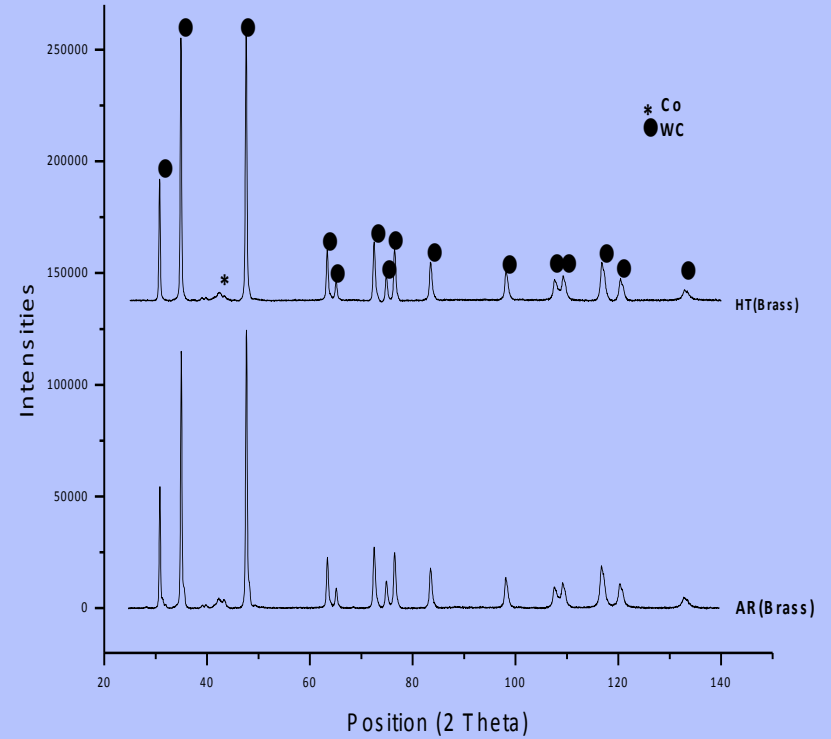
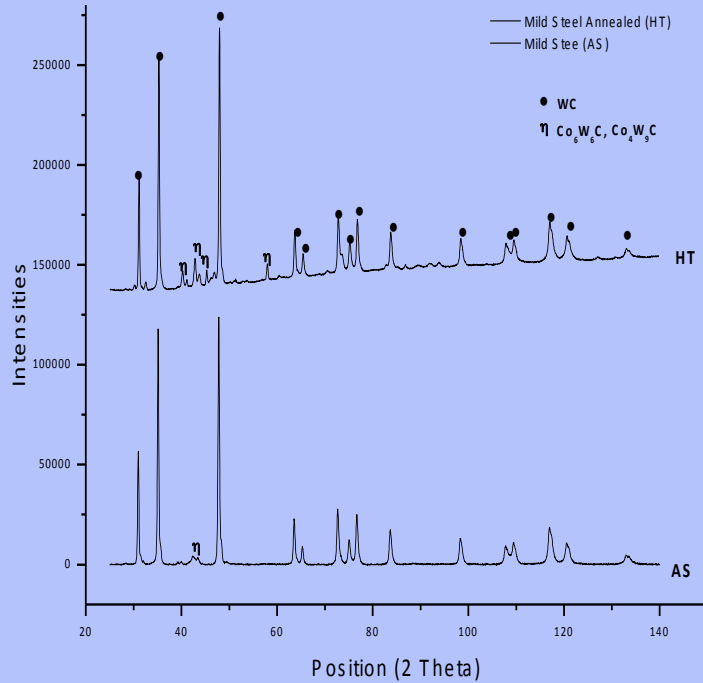


<i>Element</i>	<i>wt%</i>	<i>at. %</i>
<i>CK</i>	10.3	57.6
<i>WM</i>	77.2	28.2
<i>CoK</i>	12.5	14.2

<i>Element</i>	<i>wt%</i>	<i>at. %</i>
<i>CK</i>	12.4	59.1
<i>WM</i>	66.9	20.8
<i>CoK</i>	20.7	20.1

SEM-BSE image and EDX results of WC-Co coating on brass cross-section showing (Co) (grey), WC (light) and pore (black).

XRD results



Materials characteristics

Substrate	Wear mass loss (g)	HV Coating		Phases		Porosity (%)	WC grain size (μm)
		(GPa)		(from XRD)			
		Substrate	Coating	Substrate	Coating		
Alpha brass (Cu ₆₃ :Zn ₃₇)	0.073±0.010	1.29±0.01	6.60±0.01	Cu ₅ Zn ₃ , Zn	WC, Co	0.630±0.1	1.00±0.2
Super-invar (Fe ₆₄ :Ni ₃₆)	0.161±0.010	1.35±0.01	7.53±0.01	FeNi, C	WC, Co Co ₆ W ₆ C	0.863±0.2	0.83±0.1
Mild steel	0.084±0.010	1.25±0.01	7.01±0.01	Fe, Ni	WC, Co, Co ₆ W ₆ C	0.570±0.1	1.07±0.2
2xxx aluminium alloy	0.057±0.010	1.45±0.01	8.55±0.01	Al	WC, Co	0.618±0.1	0.94±0.2
304L stainless steel	0.066±0.010	1.74±0.02	9.11±0.01	Fe, Ni, Cr	WC, Co	0.436±0.2	1.14±0.2



Summary of residual stresses in substrates and coatings

Material	CTE	Reflection	DEC		Residual stress in grit-blast substrates		Residual stress in as-coated coatings	
	(10 ⁻⁶ /K)		(TPa ⁻¹)		(MPa)		(MPa)	
			S ₁	½S ₂	XRD	SR [6]	XRD	SR [6]
WC-17Co	2	WC (101)	-0.321	1.707	---	---	---	---
Aluminium	23	Al (3110	-5.05	19.462	-160 ± 10	-200 ± 25	-15.7 ± 17	-160 ± 50
Brass	19	Cu (311)	-2.902	11.106	-123 ± 10	-303 ± 25	-53.5 ± 28	-40 ± 25
304L SS	17	Fe (311)	-1.598	7.034	-159 ± 36	-458 ± 25	24.6 ± 19	22 ± 50
Mild steel	12	Fe (211)	-1.26	5.72	-172 ± 23	-441 ± 25	30.5 ± 19	60 ± 50
Super invar	≤ 1	Ni (200)	-1.91	7.539	-251 ± 10	-695 ± 25	74 ± 31	288 ± 25



Conclusions

- The residual stresses were tensile for the as-sprayed coatings on all substrates, except for coated aluminium and brass which were compressive. Compressive stresses were found in the other conditions due to effect of heat treatment.
- An order of magnitude correlation was found between the residual stress in the coatings determined by X-ray diffraction and Synchrotron XRD measurements, although they were fairly different due to their respective collimator or gauge volume.
- The residual stresses found on the as-sprayed coatings were quite different from each other due to their coefficients of thermal expansion.
- Moderate compressive residual stresses gave better abrasive wear resistance, whereas coatings with high tensile stresses yielded low wear resistance.

References

- [1] Oladijo O.P. *et al.* (2012). Surface Coatings Technology, 206, 4725-4729.
- [2] Gudge M. *et al.* (1991). Thermal Spray Research and Applications, ASM International, 331-337.
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- [5] Noyan I.C. and Cohen J.B. (1987) Residual Stress Measurement by Diffraction and Interpretation, New York, Springer-Verlag.
- [6] Venter A.M. *et al.* (2012) Surface Coatings Technology, 206, 4011-4020.

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