

Evaluation of WC-9Co-4Cr laser surface alloyed coatings on stainless steel

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Introduction

Results

- WC belongs to the group of advanced ceramic materials with great industrial importance and well known as hardfacing material with Co or Ni alloys as binders.
- > WC cermets decarburize with the formation of CO or CO_2 which result in the formation of pores in the coating. This could limit the wide-scale industrial recognition of this composite.
- Laser surface alloying gives a perfect adhesion of coating to the matrix with minimal heat affected zone.
- With the addition of Cr and optimum laser processing parameters, a pore and crack free coatings can be fabricated.
- Therefore, it would be of scientific and commercial interest to investigate the addition of Cr to WC cermet.



Figure 3 Microstructures of WC-9Co-4Cr powderFigure 4 SEMat different magnificationsshowing (a) Co





Figure 4 SEM and EDS results of WC-9Co-4Cr showing (a) Co-Cr binder and (b) WC



1.00

0.00

2.00

3.00

4.00

5.00



riangle FeCr

Objective

To evaluate the influence of Cr addition to WC-Co cermet by laser surface alloying.

Experimental

- A pure agglomerated and sintered WC-9Co-4Cr with average particle size of 26 μm was used as the reinforced powder.
- The surface melting operation was conducted using a 4.4 kW
 Nd:YAG laser with laser power of 2.0 kW, scanning speed of
 0.6 to 1.2 m/min, beam size of 3 mm and shield gas flow rate of
 2 L/min.
- Microstructural characterization of the coatings was performed to identify the phases present and the coating thickness.
- ➤ The Vickers hardness was determined using a 100gf load.





Figure 7 X-ray diffraction pattern of coating layer alloyed with WC-9Co-4Cr



Figure 8 Depth of alloyed layers with respect to Scan



Figure 1 Nd:YAG laser

Figure 2 Vickers Hardness tester

1.00 2.00

0.00

m/min

3.00 4.00

5.00

6.00

7.00

8.00

Figure 6 SEM image and EDS point analysis of phases

present at laser power of 2.0 KW and scan speed of 0.6

Discussion

- The variation in thickness is depended on the laser power and scan speed. At lower scan speed, the laser irradiate the sample longer, thus wide and deep melt pool forms.
- The high wettability of WC and strong convection aids the intensive mixing and uniform distribution of carbides in the melt pool.
- > The presence of undissolved carbides at the surface is due to rapid solidification of the meltpool.
- > A coated layer without cracks and pores was formed on sample a.
- Since the amount of W₂C is small, the effect of decarburization on the mechanical properties of the coating layer will be very small.
- Microhardness values obtained for the samples are 955, 816, 804 and 617 Hv_{0.1} respectively
- The different value of the hardness in the matrix was influenced by the laser speed for the entire specimen as more carbides is expected at lower scan speed.



Depth from the surface (μm)

Figure 9 Microhardness distribution of coating layers

Table 1 Hardness values

AVERAGE VICKERS HARDNESS (Hv_{0.1})

SAMPLE			
(TIC+304L)	COATINGS	MATRIX	DEPTH (µm)
a	955	246	1750
<mark>)</mark>	816	236	1260
C	804	242	1140
b	617	250	1055

Conclusions

- > 304L can be fabricated by laser surface alloying without pores and cracks at
 - laser power of 2.0 kW and scan speed of 0.6 m/min.
- The microhardness value of the matrix can be improved significantly from 246 to 1331 Hv_{0.1}